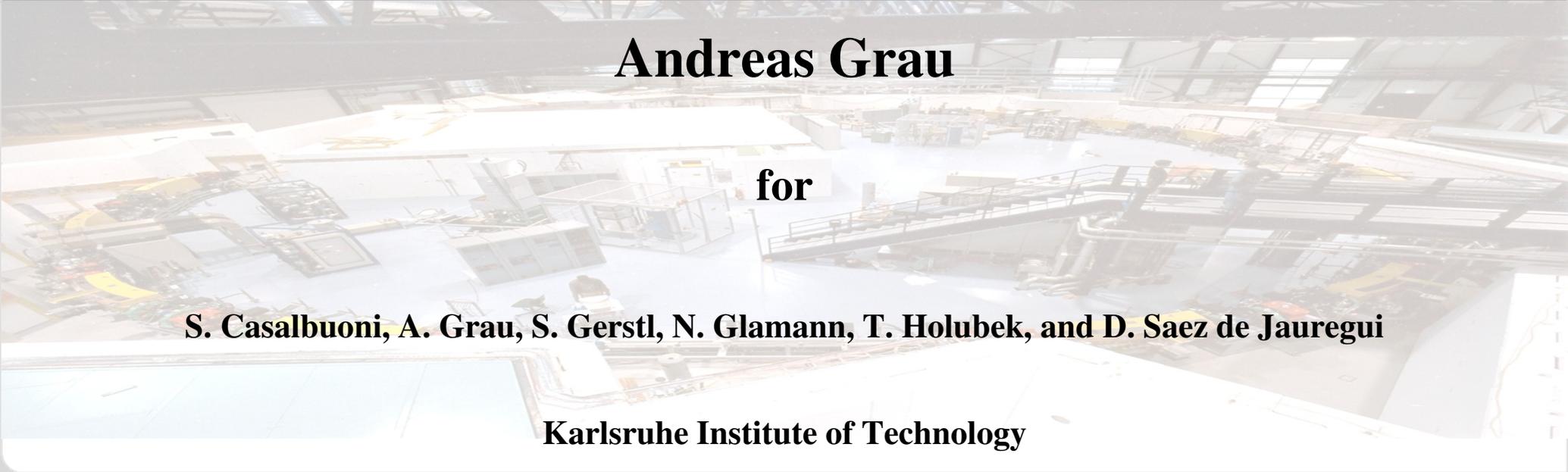


# Magnetic Field Measurement Devices for Superconducting Undulator Coils at ANKA

ANKA Synchrotron Radiation Facility



**Andreas Grau**

for

**S. Casalbuoni, A. Grau, S. Gerstl, N. Glamann, T. Holubek, and D. Saez de Jauregui**

**Karlsruhe Institute of Technology**

## 1. Introduction

- Superconducting undulators
- Motivation
- Magnetic field errors

## 2. CASPER I

- Measurement setup and equipment
- Measurement accuracies
- Measurement activities

## 3. CASPER II

- The cryostat
- Final acceptance test
- Measurement setup for local fields
- Integral field measurement setup
- Tests and upcoming work

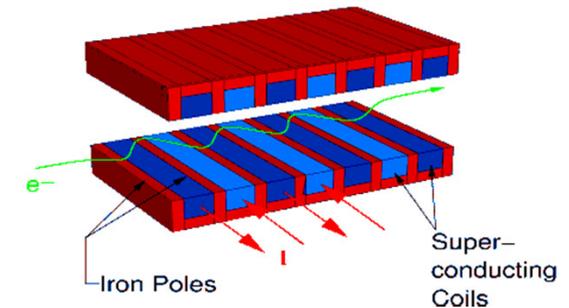
Develop, manufacture, and test superconducting undulators (SCUs) to generate:

- Harder X-ray spectrum
- Higher brilliance X-ray beams

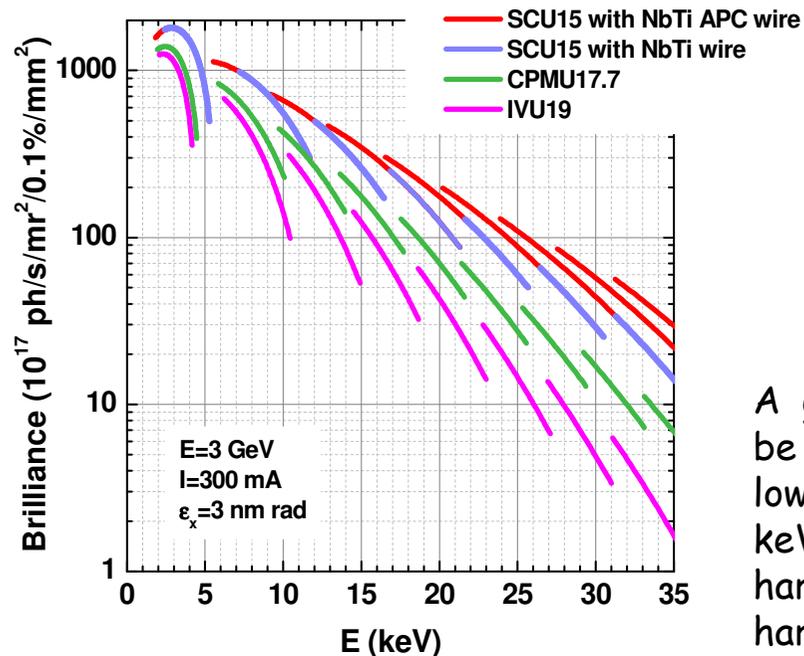
with respect to permanent magnet undulators.

Why?

Larger magnetic field strength for the same gap and period length.



Same magnetic length = 2 m and vacuum gap = 5 mm



	IVU* (SLS)	CPMU† (DLS)	SCU NbTi wire**	SCU NbTi APC††
$\lambda_u$ [mm]	19	17.7	15	15
# of periods	105	112	133	133
magn. Gap [mm]	5	5.2	6	6
B [T]	0.86	1.04	1.18	1.46
K	1.53	1.72	1.65	2.05

A given photon energy can be reached by the SCU with lower order harmonic: 20 keV reached with the 7<sup>th</sup> harm. of SCU, with the 9<sup>th</sup> harm. of CPMU and of IVU.

IVU= in-vacuum undulator  
CPMU= cryogenic permanent magnet undulator  
SCU=superconducting undulator

\* F. Bødker et al., EPAC06

† C.W. Ostefeld & M. Pedersen, IPAC10

\*\* D. Saez de Jauregui et al., IPAC11

†† T. Holubek et al., IPAC11

Task within our R&D program :

Improvement of **magnetic field properties** and quality assessment.

Magnetic errors can cause:

Perturbation of the closed orbit and the dynamics of the electron beam

➔ **Field integral measurements are needed**

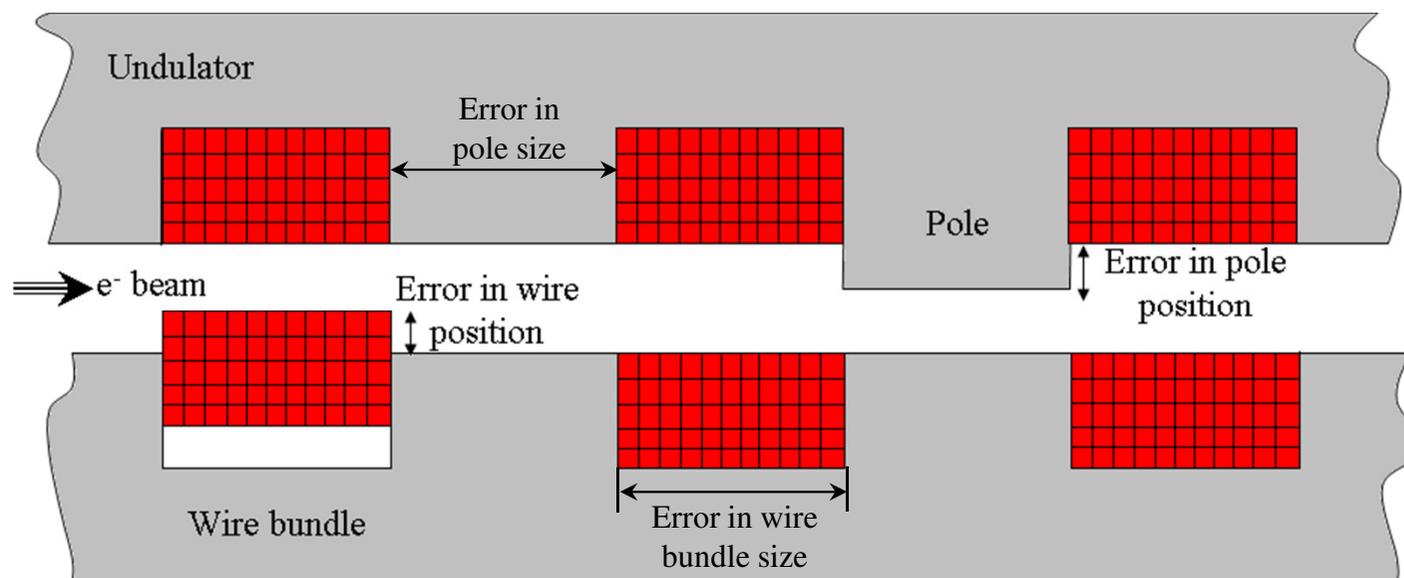
Reduction of the quality of the emitted radiation

➔ **Perform local field measurements to obtain phase error**

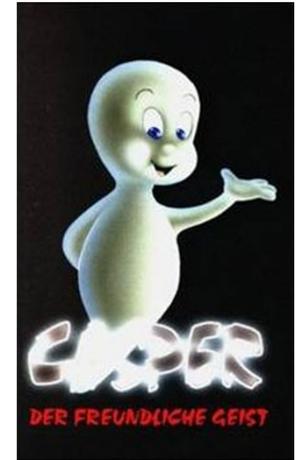
# Main errors in superconducting undulators

Field errors are mainly caused by:

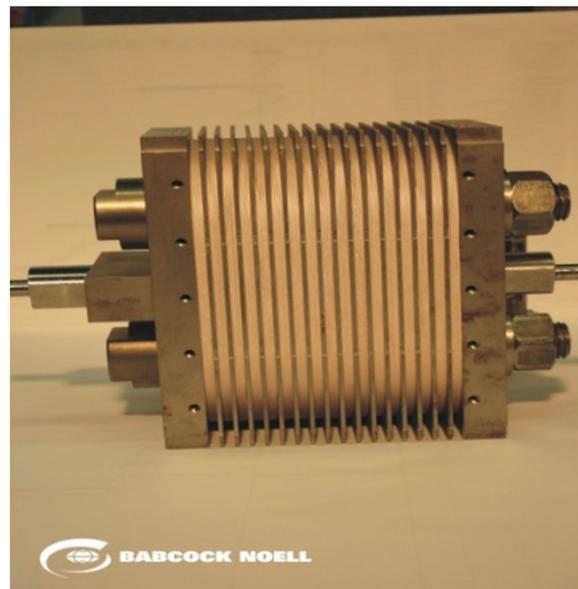
- Mechanical deviations of the pole position e.g. the pole height
- Deviations in the period length
- Bending of the yoke
- The position of the superconducting wire bundles
- Pole and wire bundle size



# CASPER - Characterization Setup for Field Error Reduction



**CASPER I** - Measurement setup for short undulator mock-up coils



**CASPER II** - A measurement system for undulator coils up to 2m length

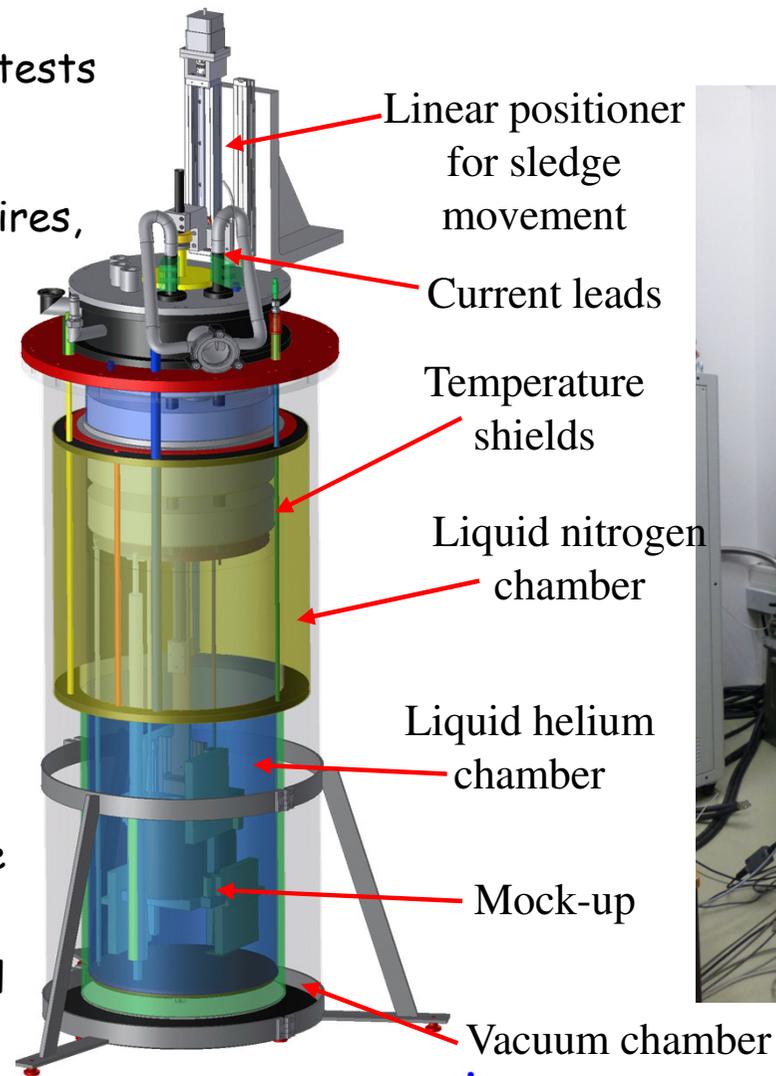
- Perform magnet training and quench tests
- test new winding schemes,
- new superconducting materials and wires,
- and new field correction techniques

### General:

- Operating vertical
- Test of mock-up coils in LHe
- Maximum dimensions 35cm in length and 35 cm in diameter

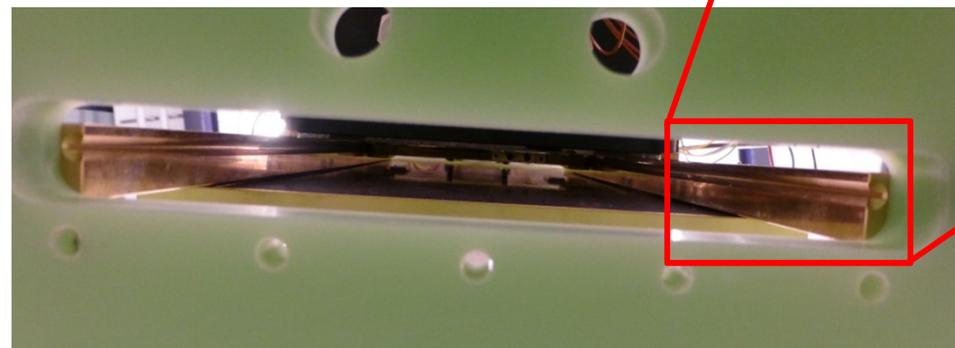
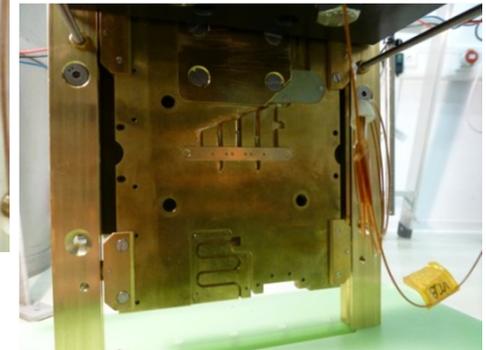
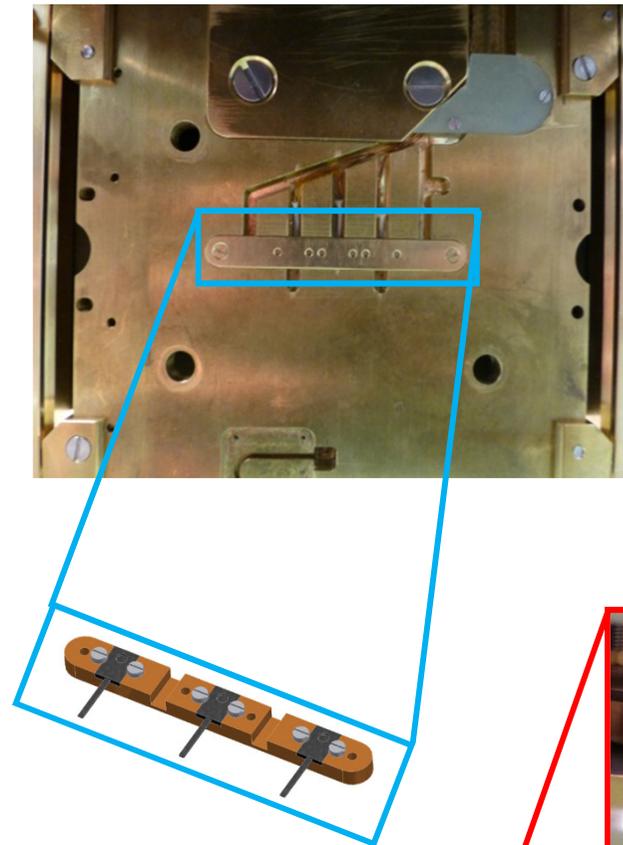
### Instrumentation:

- Keithley constant current source (Hall current)
- Keithley multiplexer voltmeter (Hall voltage)
- 1500A/±5V and 500A/±5V power supplies providing coil operating currents
- Quench detector for coil protection
- Data logging system for quench analysis



E. Mashkina et al., EPAC08

- Magnetic field distribution measured with Hall samples
- 3 calibrated Hall samples clamped to a holder and mounted to the sledge
- One in the middle and two at  $\pm 10\text{mm}$  perpendicular to the beam axis to measure roll off
- Sledge moved from outside by a linear stage with stepper motor, gear box and a low expansion coefficient non magnetic tube (system resolution  $3\ \mu\text{m}$ )
- Sledge guiding via brass rails



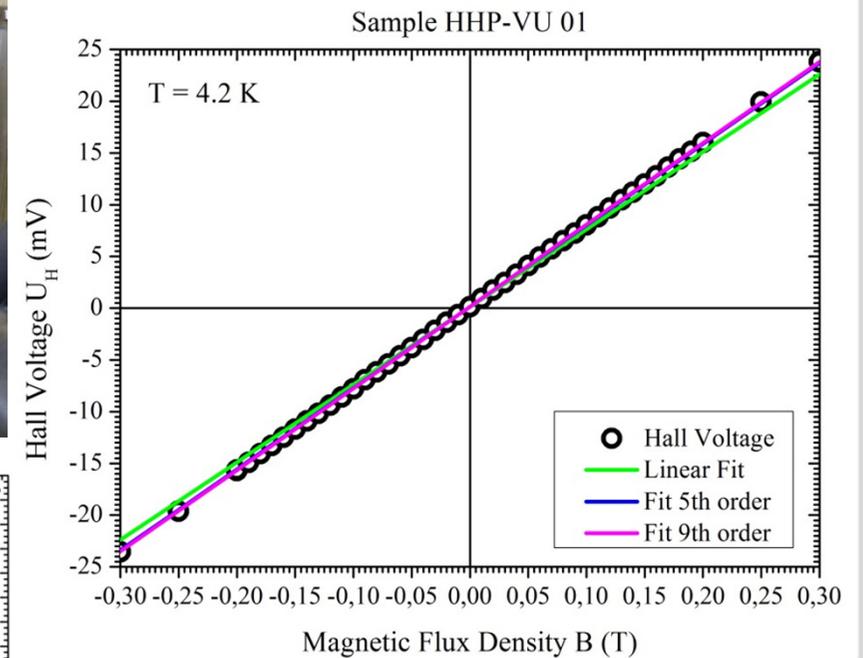
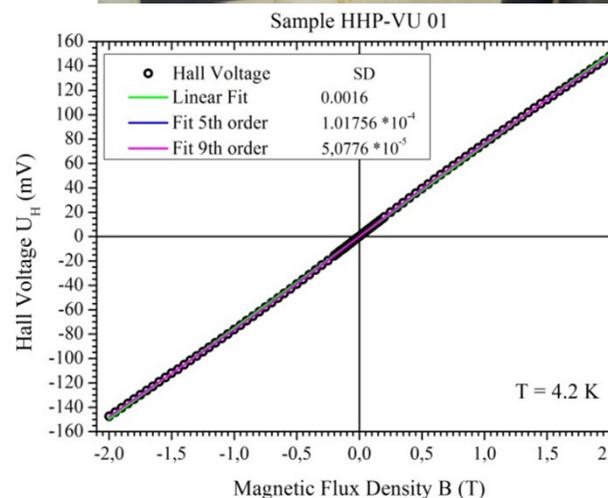
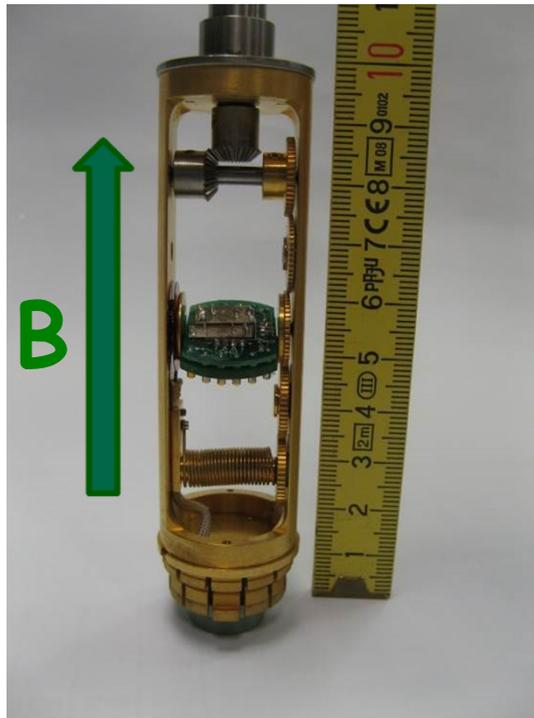
## Errors effecting local field measurements

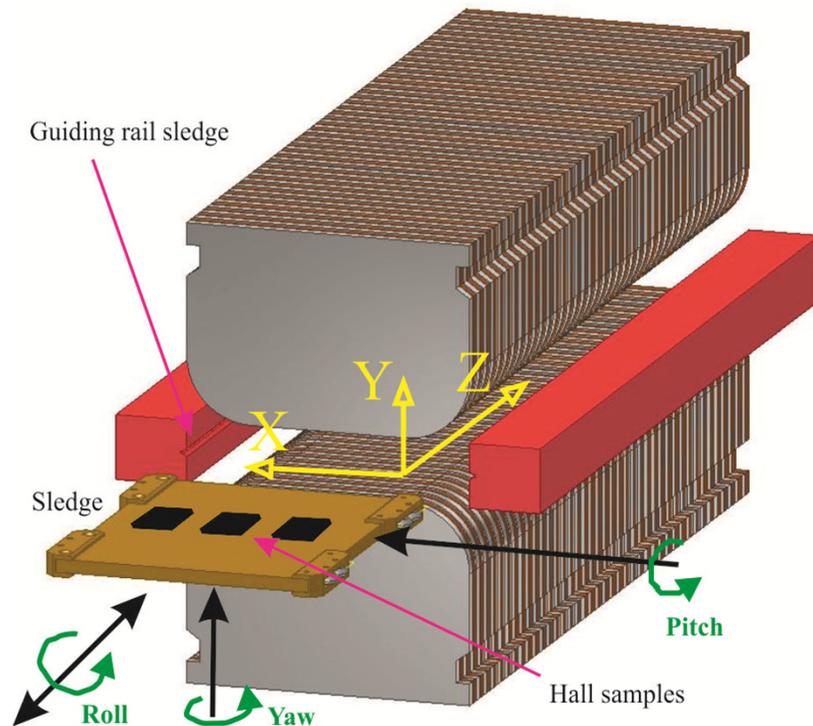
1. Errors caused by Hall sample calibration.
2. Measurement errors due to mechanical misalignment of the guiding rails or the field sensors

Physical Properties

Measurement System

Hall sample calibration  
(ITeP at the KIT)





Relative alignment precision of guiding rails  $20\mu\text{m}$ .  
For the Hall probe in the middle the distance to coils changes by  $10\mu\text{m}$ .

In x-direction the field is fairly uniform  
 ➔ error is negligible

In y-direction the  $10\mu\text{m}$  yields according to [1] with  $\lambda_u=0.015$  to:

$$\cosh\left(\frac{2\pi\Delta y}{\lambda_u}\right) = 1 + \frac{\Delta B}{B} \quad \Delta B/B = 9 * 10^{-6}$$

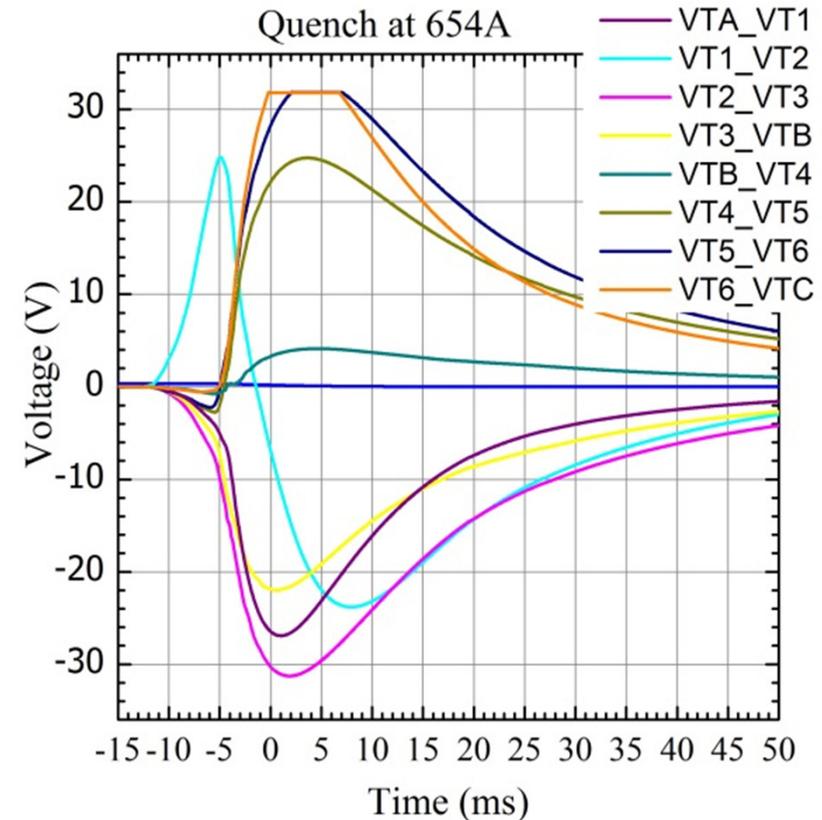
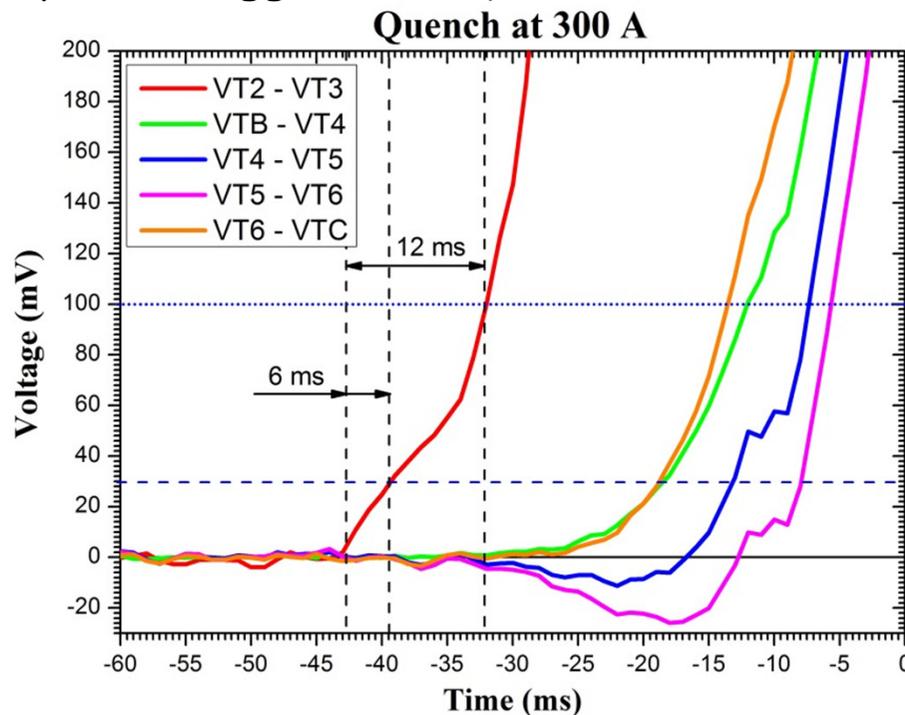
In longitudinal direction  $\Delta z < 5 \mu\text{m}$

The angle errors cause a  $\Delta B/B < 5 * 10^{-8}$

[1] Zachary Wolf, "Requirements for the LCLS Undulator magnetic measurement bench", Technical report # LCLS-TN-0, 4-8 <http://www-ssrl.slac.stanford.edu/lcls/technotes>

## Quench tests and analysis

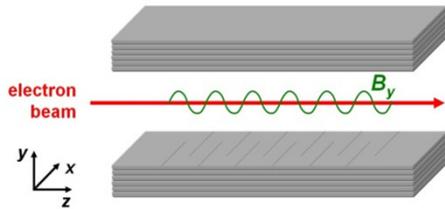
- Test coils electrically divided in sections (Voltage taps)
- Data logging system with 16 Channels (100 kS/s max., Company IMC )
- System trigger from quench detector



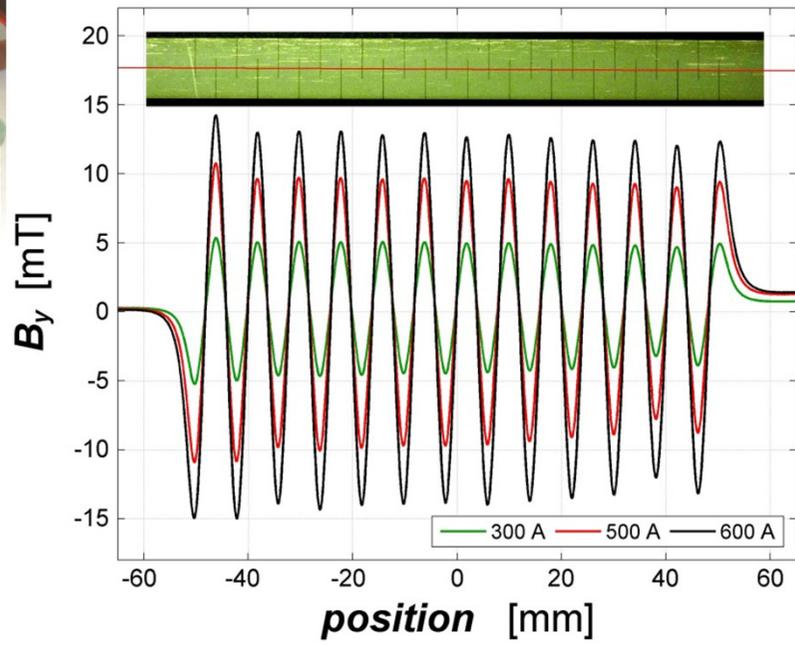
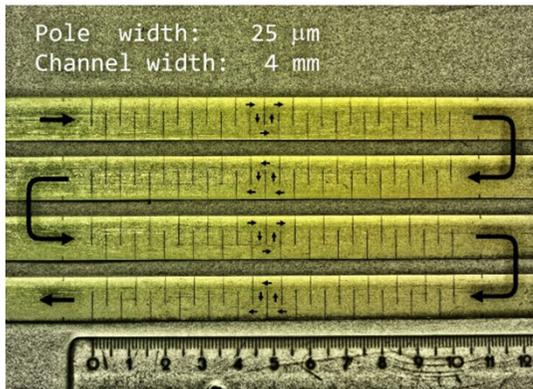
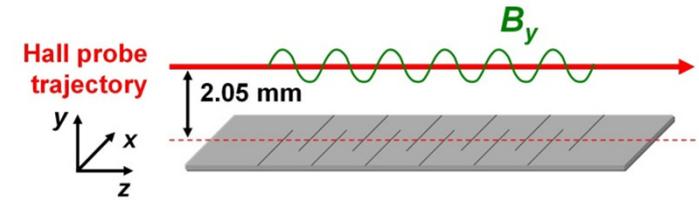
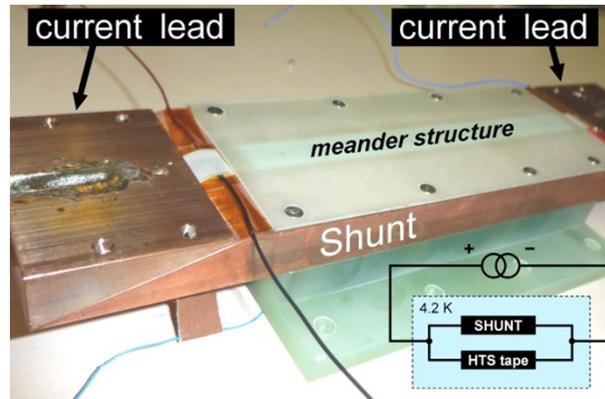
## Tests and measurements on structured HTS tapes

Idea: To build an undulator out of stacked structured HTS tapes

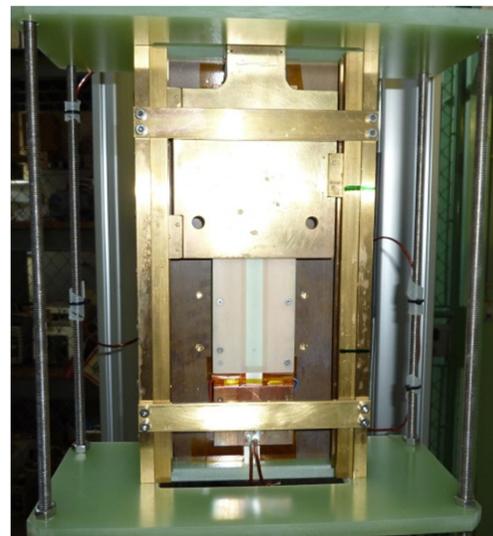
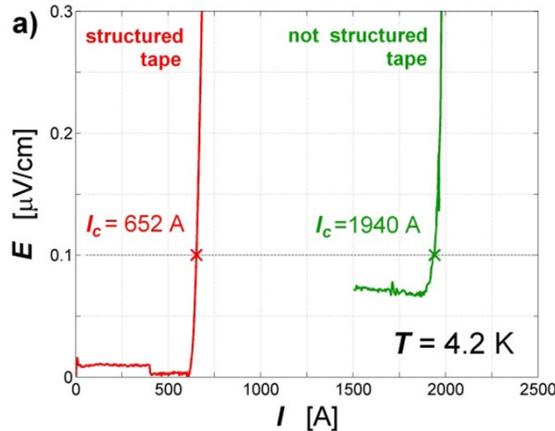
S. Prestemon et al., IEEE Trans. on Appl. Supercond., Vol 21, No. 3, 1880-1883 21-3 (2011)



### Perform field measurements



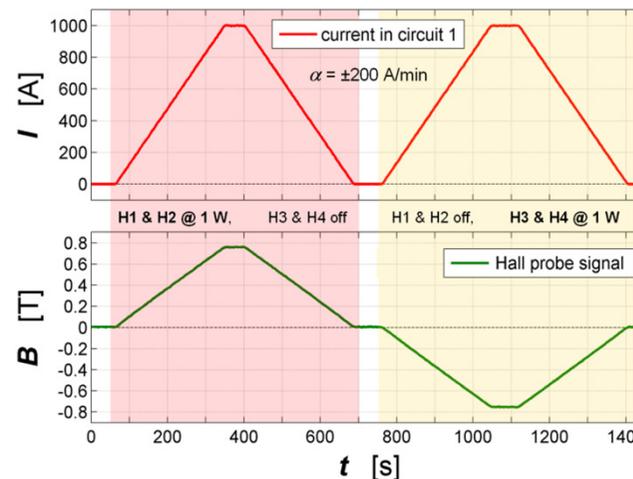
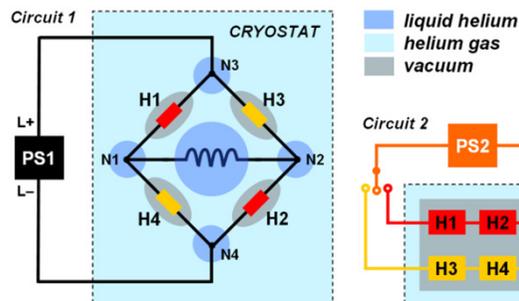
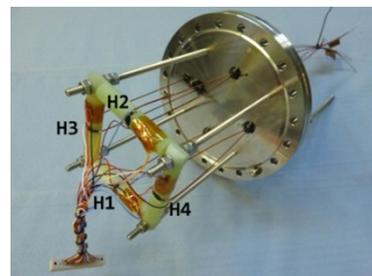
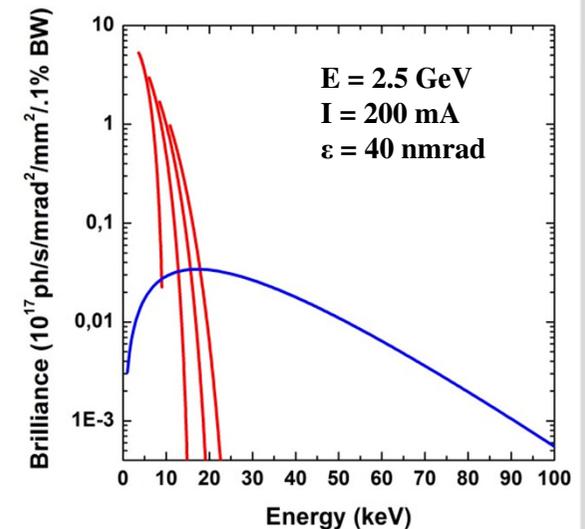
### Test maximum current



T. Holubek et al., IEEE Trans. on Appl. Supercond. Vol. 23, No. 3, 4602204 (2013)

## Superconducting switch (SCS)

- Switching the period length allows to increase the tunability of an insertion device
- Superconducting undulator/wiggler (SCUW 18/54) planned for the IMAGE beamline at ANKA
  - High brilliance of the undulator 6keV to 15keV for imaging, wiggler mode for higher photon energies (phase contrast tomography)
- Current has to be reversed in a separately powered subset of the windings
- Use SCS instead of two power supplies (conduction cooled)



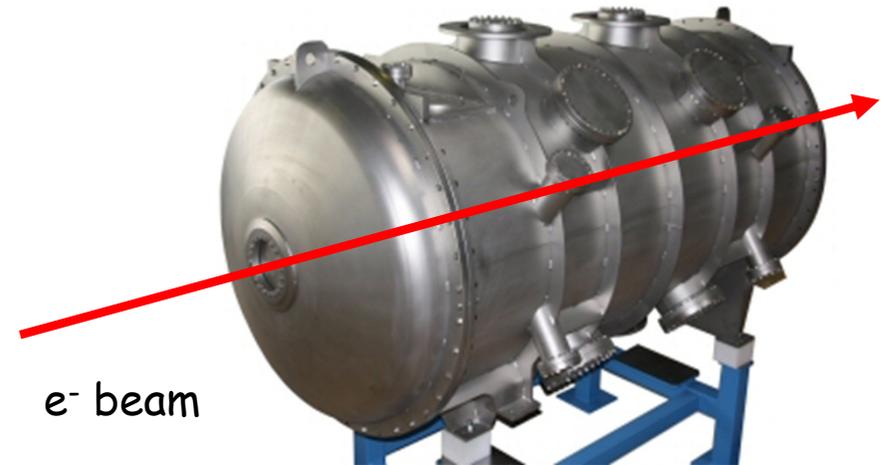
Finally the heating power was reduced to 200mW per heater pair.

T. Holubek et al., IEEE Transactions on Appl. Superconductivity, Vol. 23, No. 3, 3800104 (2013)

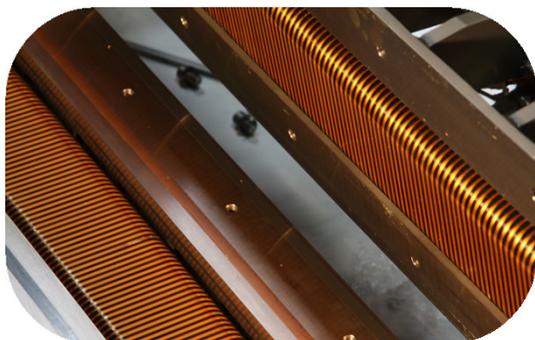
[1] R. Schlueter, S. Prestemon, Synchrotron Radiation News, 2004

## Light source under development in collaboration with BNG for the beamline NANO at ANKA

Period length	15 mm
Number of full periods	100.5
Max field on axis with 5.4 mm magnetic gap	1.43 T
Max field on axis with 8 mm magnetic gap	0.77T
Max field in the coils	2.4 T
Minimum magnetic gap	5.4 mm
Operating magnetic gap	8 mm
Operating beam gap	7 mm
Gap at beam injection	16mm
K value at 5.4 mm magnetic gap	2
Design beam heat load	4W



Delivery end of 2013

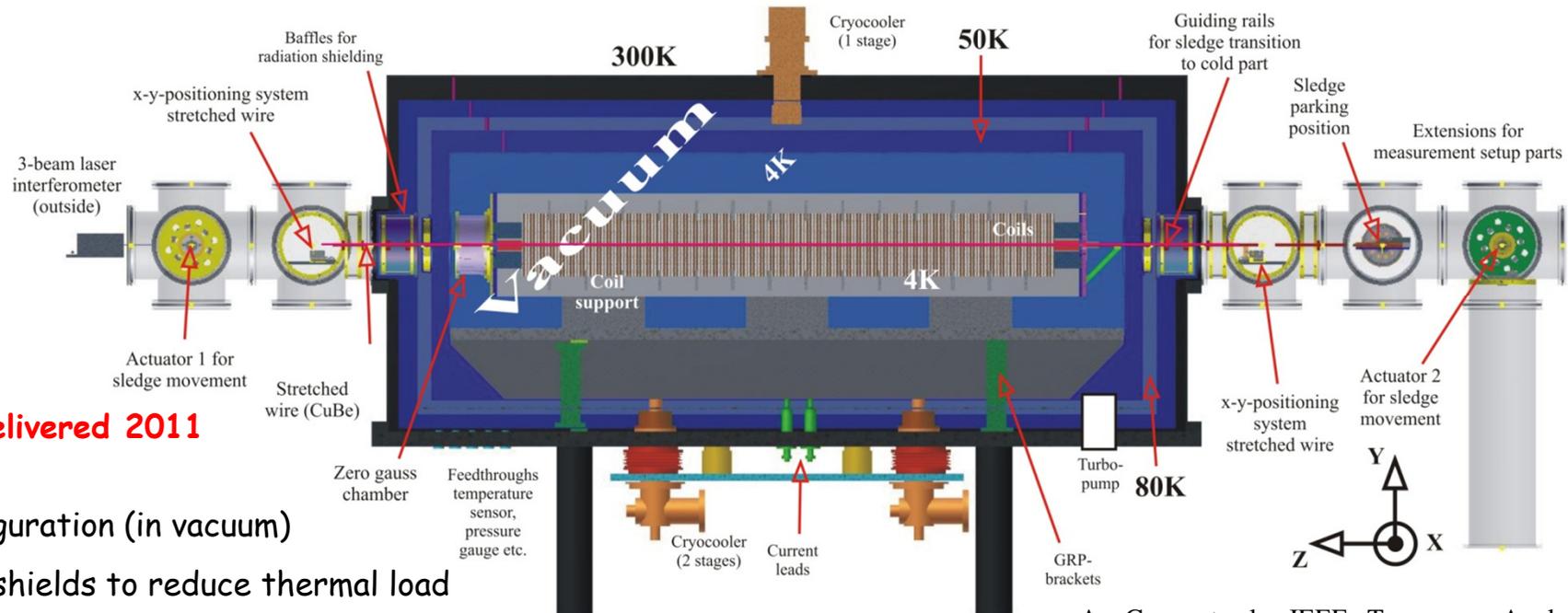


C. Boffo et al., IEEE Trans. on Appl. Supercond Vol. 21, No. 3, 1756-1759 (2011)



## The goal...

Measure magnetic field distributions of superconducting coils with dimensions like in „real“ IDs (e.g. up to ~2 m length, ~50cm diameter)



**Cryostat delivered 2011**

- Vertical configuration (in vacuum)
- Temperature shields to reduce thermal load
- Partially cryogen free :
  - ➔ To 4K via cryocooler
  - ➔ precooling 4K plate and thermal shields (80K) with liquid N<sub>2</sub>
- Dimensions 4K region 2m x 0.5m x 0.5m
- Current leads 8 x 500A, can be variable connected
- Local and integral field measurements possible, access through the flanges

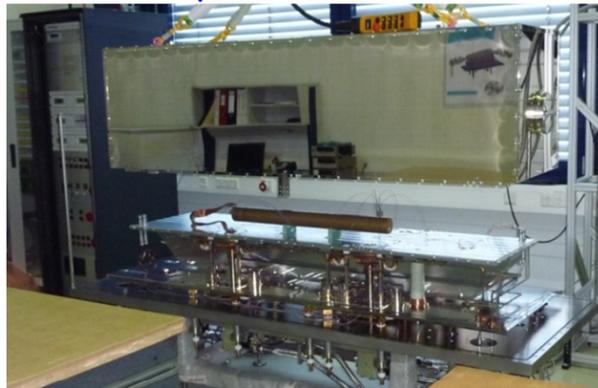
A. Grau et al., IEEE Trans. on Appl. Supercond., Vol. 22, No. 3, 9001504 (2012)

For **quality certification** of new sc-insertion devices developed together with the industrial partner Babcock Noell GmbH.

4K plate & base plate



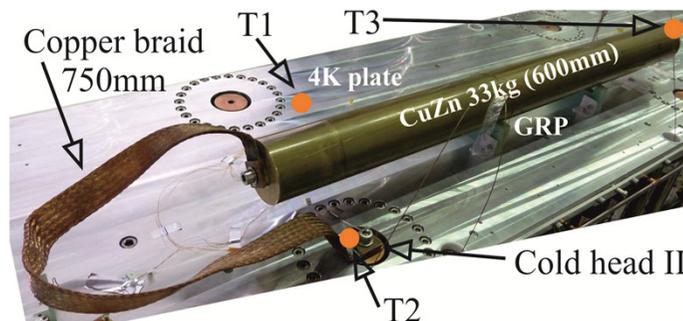
4K plate & 50K shield



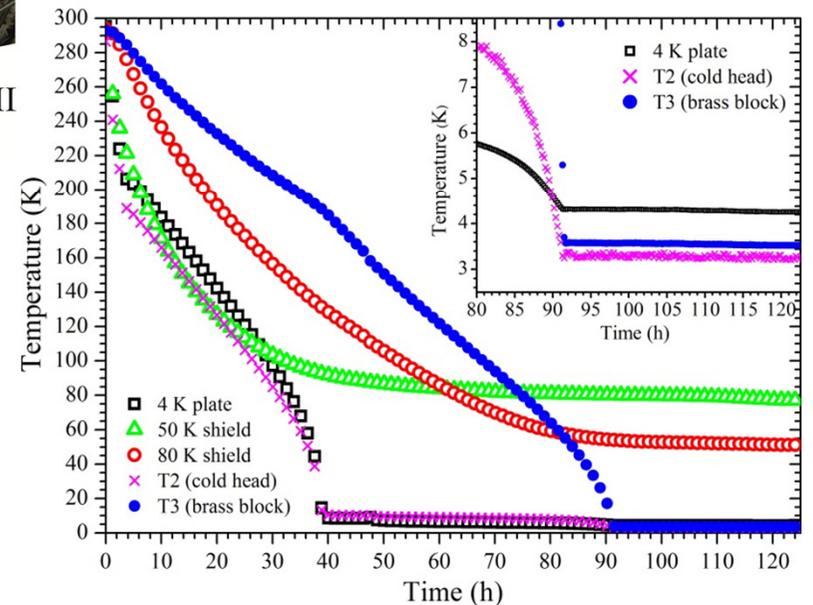
Complete

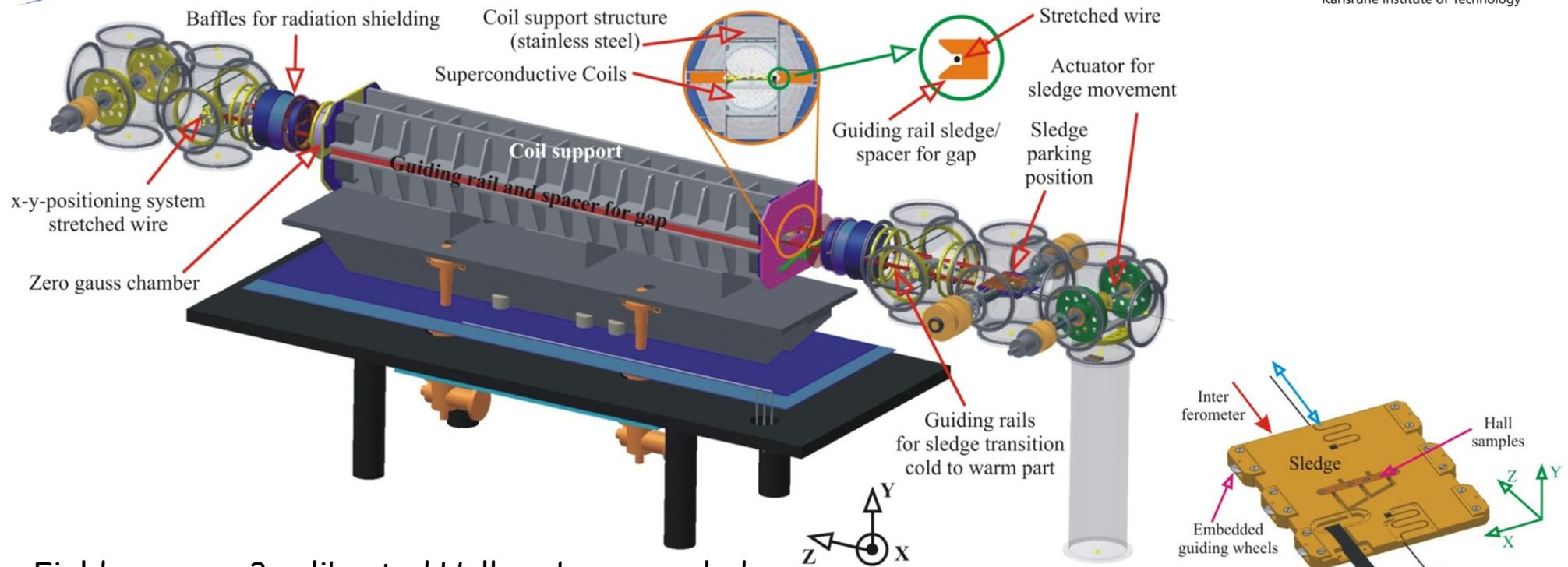
## Final acceptance test

Testsetup to simulate temperatures in 4K region.



Component	Specified value	Reached value
Temperature 80K-plate	T < 85 K	Ø 83 K
Temperature 80K-shield	T < 100 K	Ø 81 K
Temperature 50K-shield	T < 60 K	Ø 46 K
Temperature 4K-shield	T < 10 K	Ø 5.2 K
Temperature 4K-plate (T1)	T < 4.5 K	Ø 4.8 K
T2	targeted < 4 K	3.3 K
T3	“	3.5 K





- Field sensors: 3 calibrated Hall probes on a sledge
- Hall current provided by a Keithley precision current source
- Hall voltage measured with a Keithley multichannel voltmeter
- Field integral measurements with stretched wire technique (CuBe wire  $\varnothing 125\mu\text{m}$ )
- Position adjustment for stretched wire in x-y-direction via linear piezo stages with encoders (precision  $\sim 1\mu\text{m}$ )
- Position measurements with a 3 beam laser interferometer (SIOS)
  - Precise z-position  $\Delta z \sim 10^{-6}$
  - Values for angle deviation of the sledge during movement

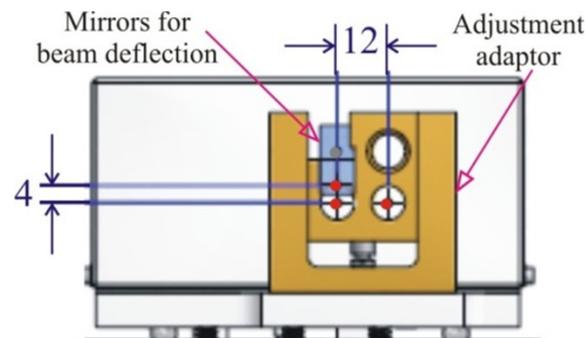
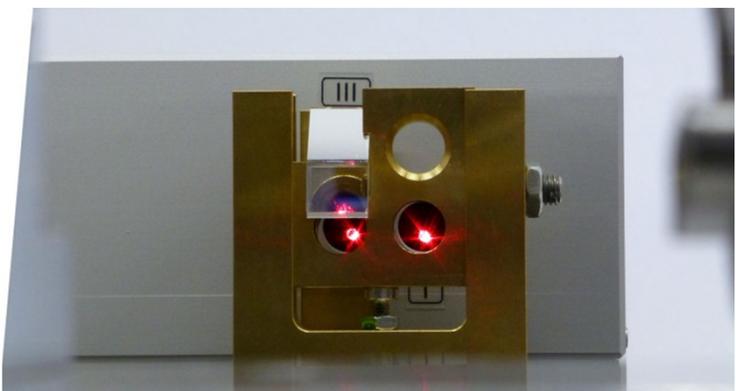
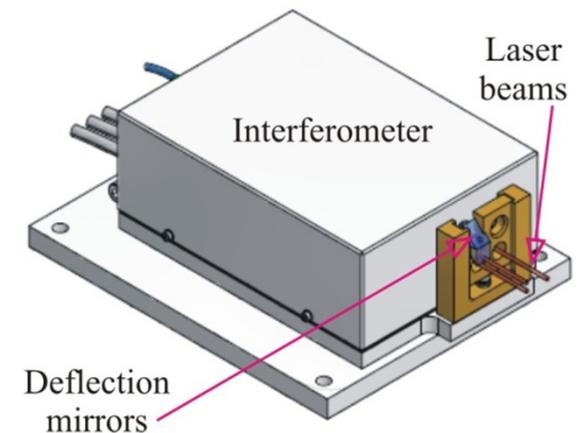
## Laser interferometer (3 beams)

- ♦ Measure z-position of the sledge (1 beam)
- ♦ Angle deviation during moving (3 beams)

Usable gap in the undulator max. 7mm.

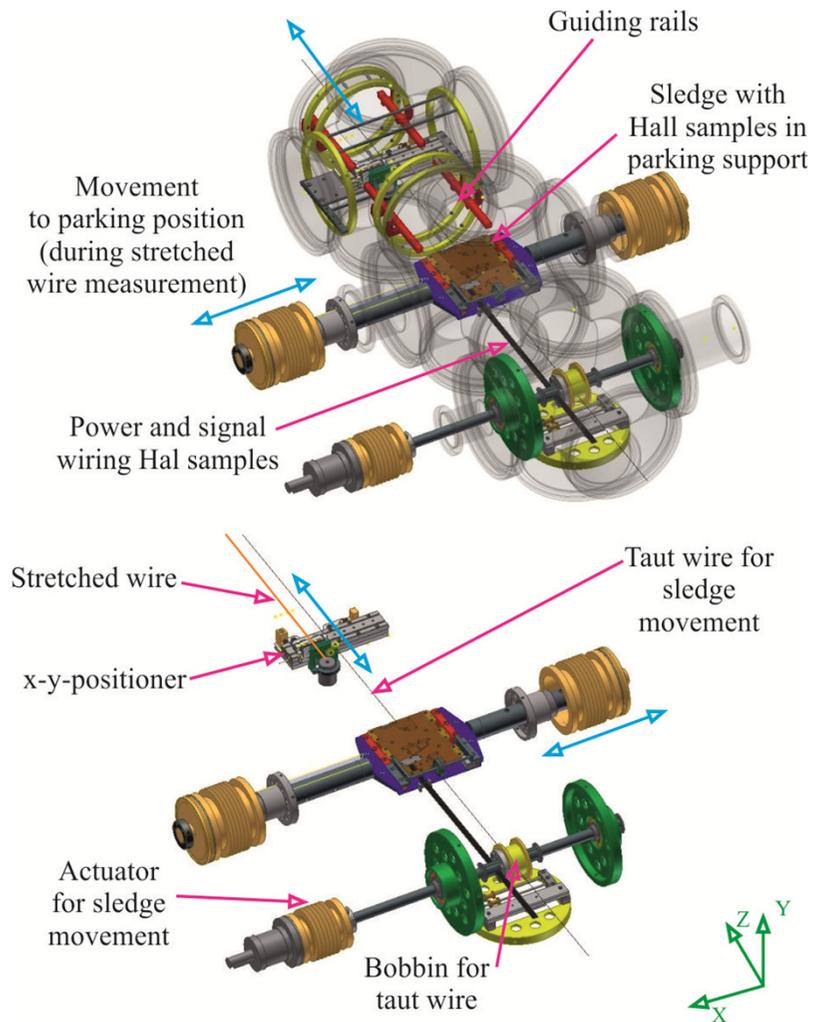
- ➔ Beam distance has to be reduced from 12mm, because usable gap in the undulator max. 7mm

Commercial interferometer with two prisms attached for beam distance rescaling.

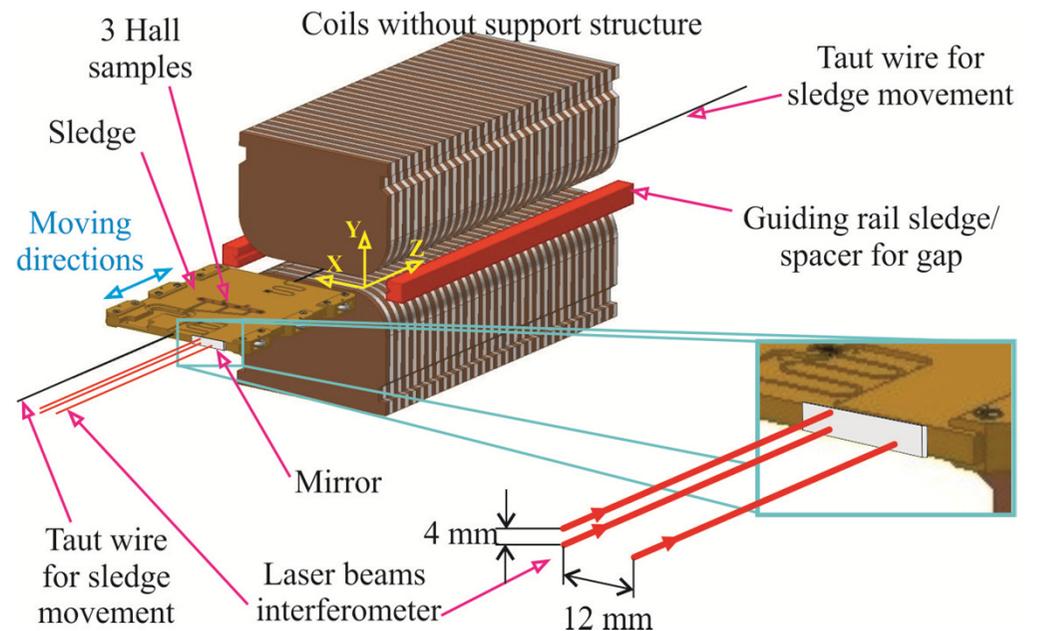


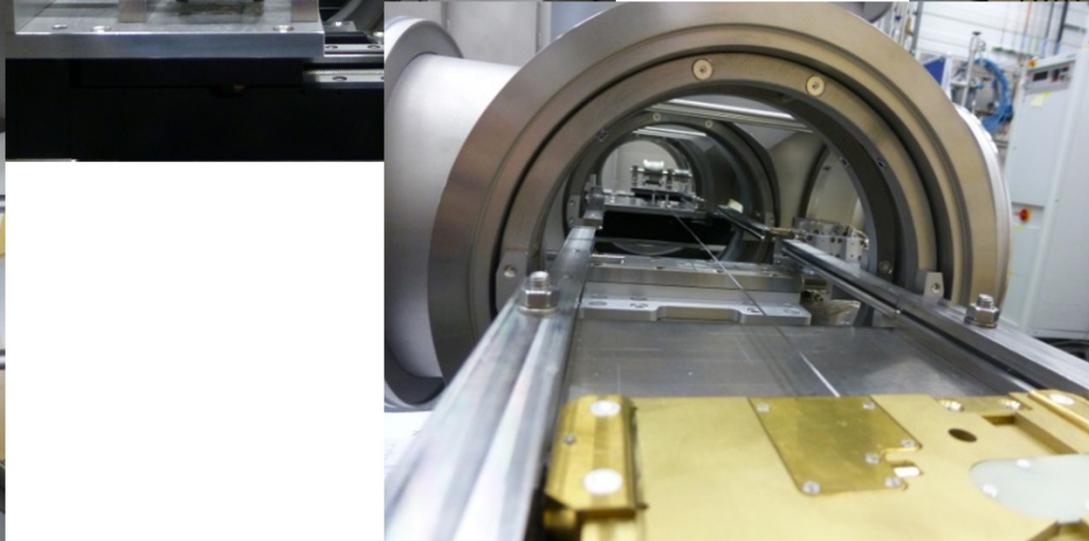
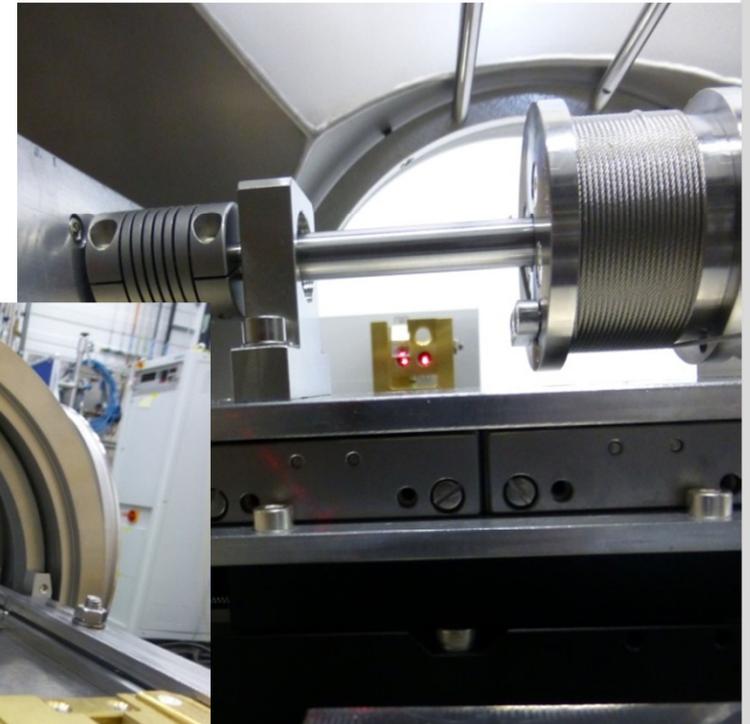
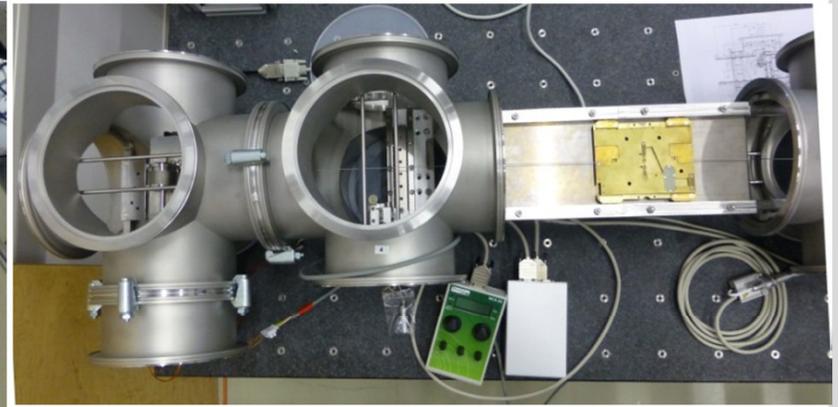
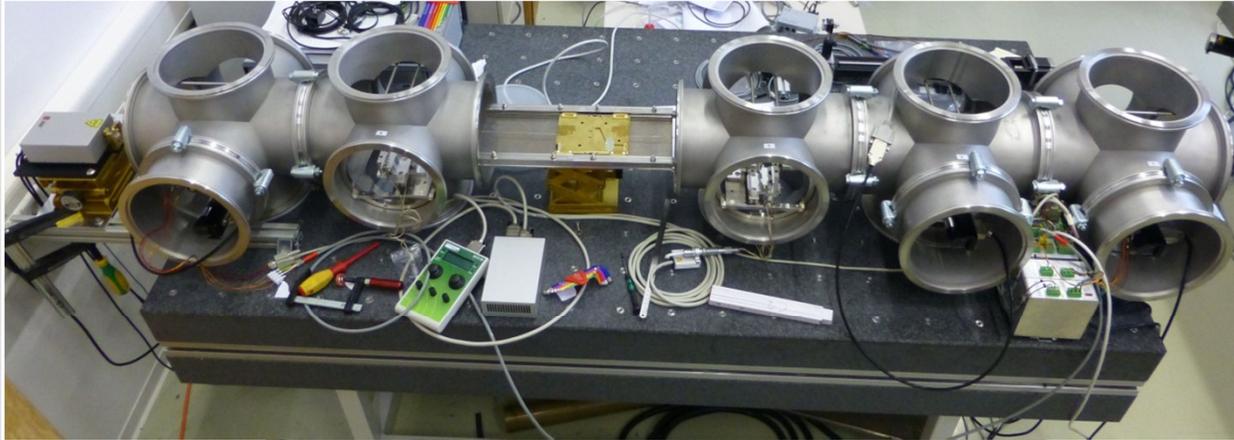
Company SIOS

3 Hall probes in a row placed perpendicular to beam axis (10mm distance)

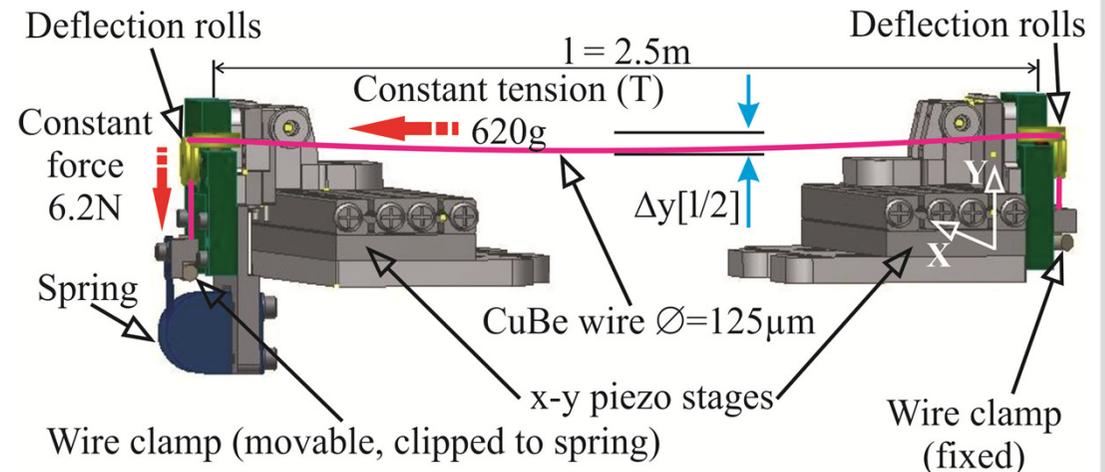


Sledge movement by a taut wire for each direction spooled on a bobbin at each side mounted in the extensions of the cryostat.





- Copper Beryllium wire
- Diameter  $125\mu\text{m}$
- Length through the whole cryostat  $\sim 2.5\text{m}$
- Movable along 2 axes (150mm x-axis, 20mm y-axis) synchronous or opposite directions



## Error consideration

Accuracy limit is set by the sag  $\Delta y$  in the middle ( $l/2$ ) of the wire and depends on the tension and the self-weight [1]

$$\Delta y\left(\frac{l}{2}\right) \cong -\frac{\omega_{\text{CuBe}} l^2}{8T} = -82\mu\text{m}$$

With  $\varnothing_{\text{CuBe}} = 125\mu\text{m}$ ,  
 $\omega_{\text{CuBe}} = 0.064\text{g/m}$ , and  
 $\lambda_U = 0.015\text{m}$

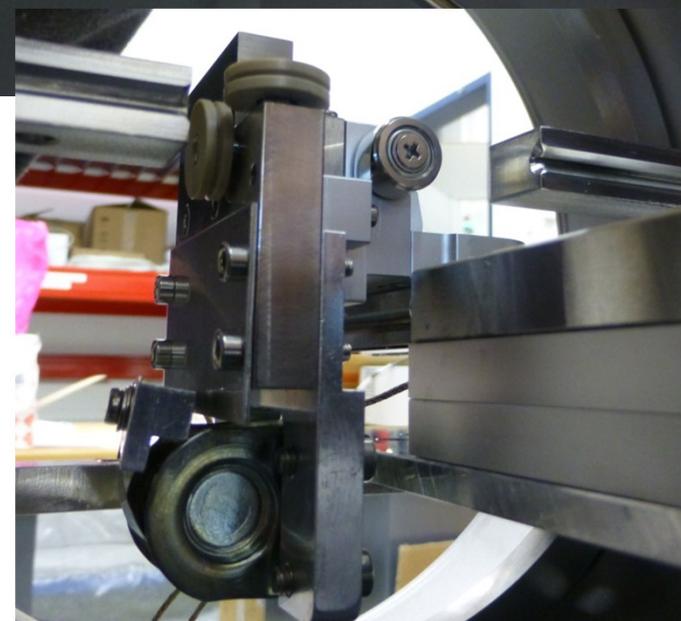
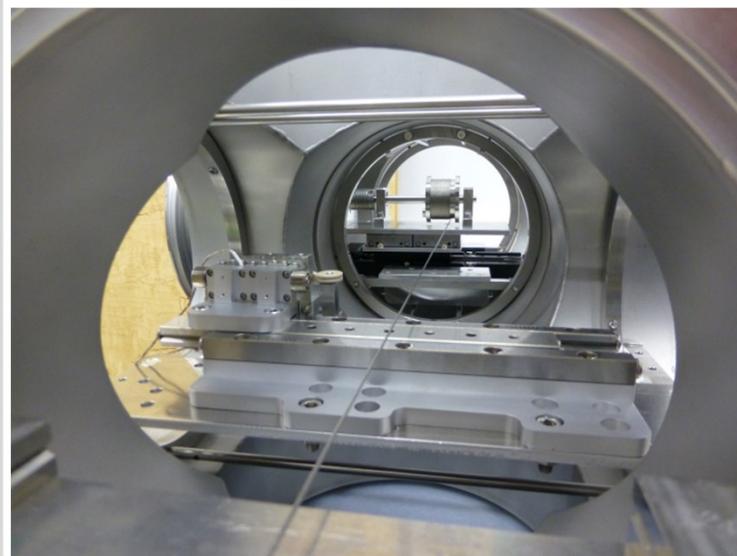
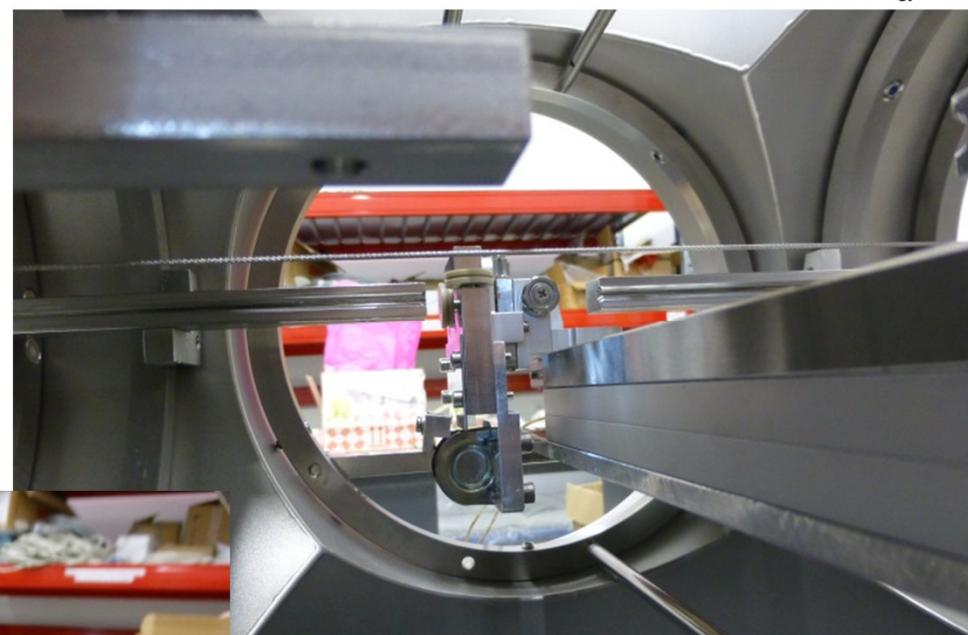
Resulting Error in the field integral from [2]

$$\frac{\Delta I_y}{I_y} \approx \frac{1}{2} \left( \frac{2\pi}{\lambda_U} \right)^2 \cosh\left( \frac{2\pi}{\lambda_U} \Delta y \right) (\Delta y)^2 \approx 5.9 \times 10^{-4}.$$

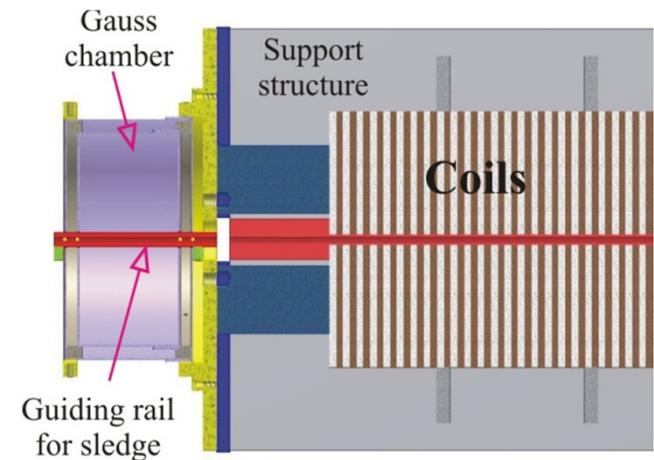
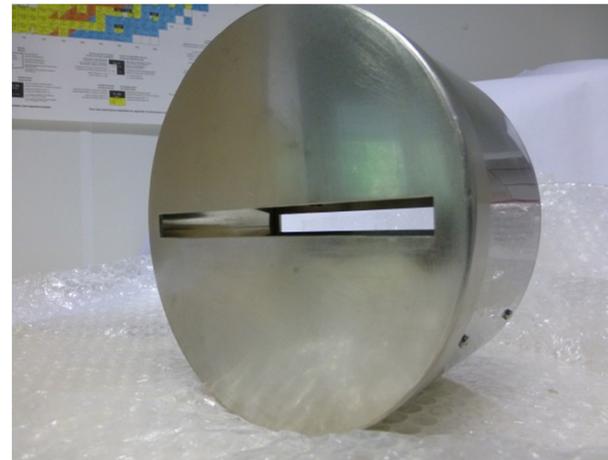
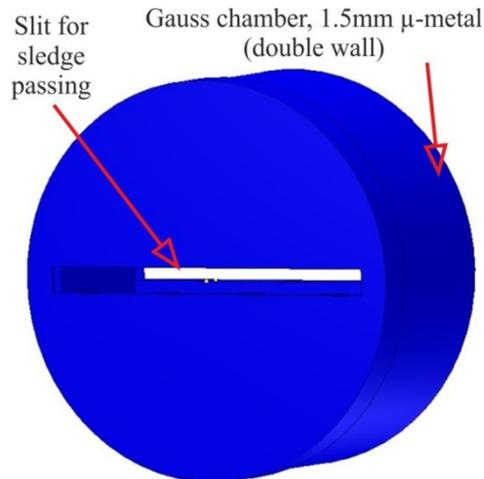
- Result for sag checked with a testsetup with  $l=2\text{m}$  and  $T=620\text{g}$ .
- Vertical distance between the CuBe wire and table surface at both ends and in the middle of the wire measured with gauge blocks.
  - ➔ yielded to a sag of  $\Delta y = 50\mu\text{m}$ .
  - ➔ good agreement with  $\Delta y = 53\mu\text{m}$  from calculations [1]

[1] G. Bowden "stretched wire mechanics," Technical report, #SLAC-Pub-11465, Stanford Linear Accelerator Center, 2004

[2] F. Ciocci et. Al. „some considerations on the SPARC undulator magnetic measurements," Technical report #SPARC-FEL-06/001, ENEA Frascati, 2006

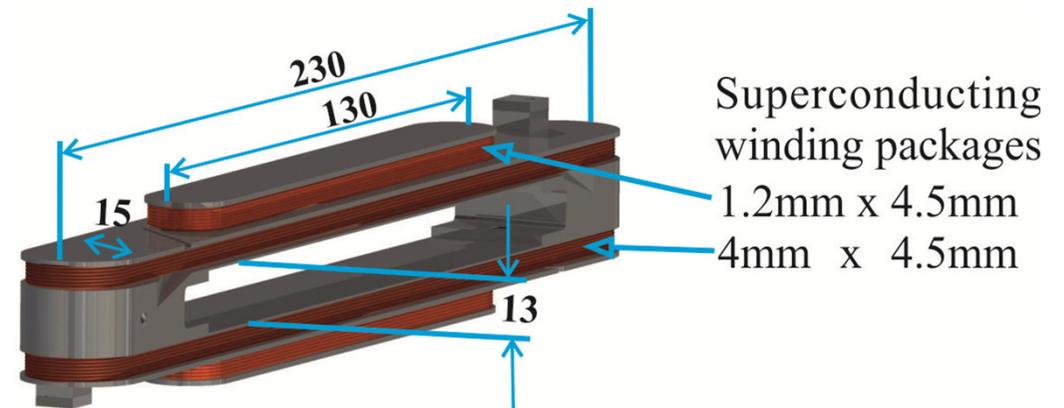


Field shielding chamber to adjust the zero-point of Hall samples when cold



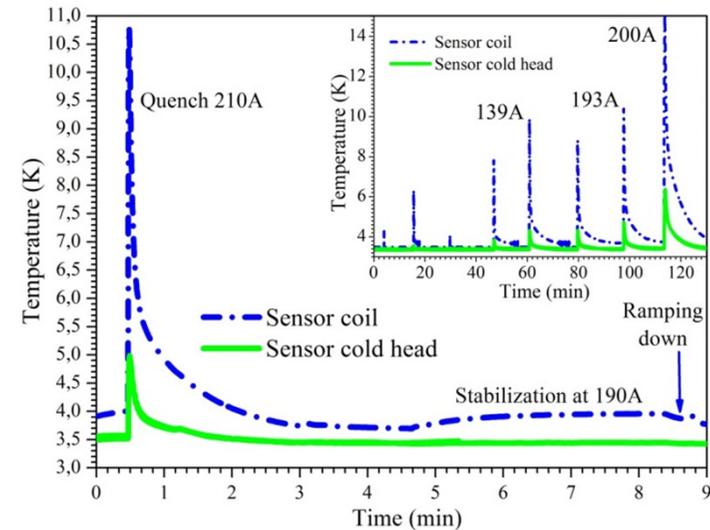
Stacked racetrack coils mounted in Helmholtz configuration to check calibration curve of the Hall samples

- Field at  $I=400A$  in the SC wire 650mT
- Field homogeneity over 20mm in the center 0.15mT
- In the design phase, improvement possible
- Design and winding at KIT

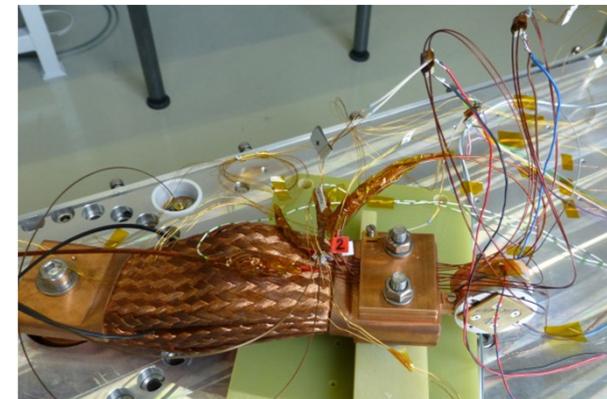
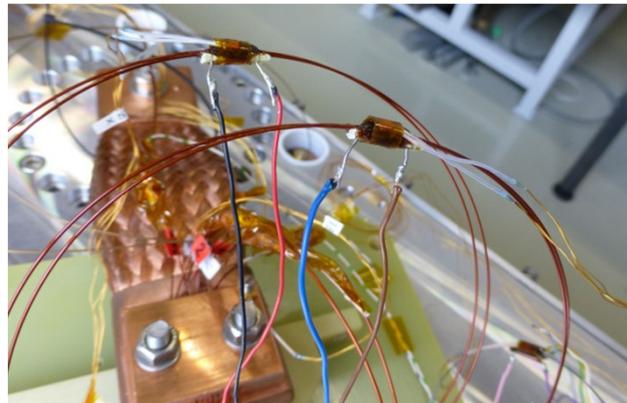


## First quench tests with a conduction cooled test coil

- Conduction cooling is performed like for the final device connected via a copper braid (560mm<sup>2</sup>) to a coldhead
- Temperature reached at the superconductor 3.6K with a gradient of 0.2K to the coldhead
  - Improved connection compared to the FAT
- Reached 200A after a few quenches
- Time to recover from quench ~5min.
- At higher currents (210A) a quench occurs due to superconductor warming (joints)
- Stable cooling possible up to 190A
  - Well above the operation current 155A



Test SCS in vacuum and conduction cooled



## **Mechanically**

- Final alignment of the guiding rails in the cryostat extensions
- Alignment of the extension parts to each other and fixation
- Final preparation of the sledge for measurements (Hall samples, wiring etc.)
- Alignment of moving stages in the cryostat extensions
- Adjustment of Stretched wire parts
- Define fiducial points at the measurement system for alignment at the cryostat
- Completion of the support structures for the measurement parts
- Assembling of measurement system and cryostat

## **Software programming (LabView)**

- Two rotating stepper motors for sledge movement
- Three Linear stages
- Laser Interferometer
- Two x-y axis piezo stages for stretched wire measurements
- Data recording from Hall samples and stretched wire
- Power supplies for main current
- Data acquisition system up to 64 channels, sampling rate 250 kS/s
- Data processing for quench analysis



# Acknowledgements



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**IPE**

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W. Walter**

**Fa. CryoVac  
Fa. SIOS  
National Instruments**

Karlsruhe  
Institute of  
Technology

Babcock Noell GmbH

... and to you for your attention !

